



STAFF REPORT

PLANNING DIRECTOR DECISION

DATE: September 18, 2009

FILE NO.: MISC-09-11 (Planning Directors Decision)

SUBJECT: Request to replace an existing, nonconforming deck on the same footprint, with the addition of one wall and a roof which would constitute an expansion of a nonconforming structure.

PLANNER: Tom Soppe, Associate Planner

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SPECIFIC DATA

OWNER/

APPLICANT: Richard Ahyou, 2155 5th Ave., West Linn, OR 97068

CONSULTANT: Todd Larios, 4804 NE 7th Avenue, Portland, OR 97211

SITE LOCATION: 2155 5th Avenue

SITE SIZE: Approx. 10,435 sq. ft.

LEGAL

DESCRIPTION: 3 1E 02AB, Tax Lot 5700

COMP PLAN

DESIGNATION: Low-Density Residential

ZONING: R-10, Single-Family Residential

APPROVAL

CRITERIA: CDC Chapters 66 Nonconforming Structures

120-DAY RULE: The application was declared complete on August 31, 2009. The 120-day period therefore ends on December 29, 2009.

PUBLIC NOTICE: Notice was mailed to property owners within 100 feet of the subject property and the Willamette Neighborhood Association on September 3, 2009. The notice was also posted on the City's website. Therefore, public notice requirements of Community Development Code Chapter 99 have been met.

EXECUTIVE SUMMARY

The subject house, located in the R-10 zone in the Willamette neighborhood, is a nonconforming structure in that the west side of the house is less than 7.5 feet from the side property line as required by CDC Section 11.070 (5) (b). Most of the house and an existing elevated deck are located 5 feet from the western side property line (see the attached site plan, Exhibit PD-4, page 37). However, a small area at the front of the house is only one foot from the side property line and one small "bumpout" near the rear of the house is approximately 3 feet from the property line. Per CDC Section 38.060(F), the existing deck is nonconforming as well as the house; in that decks over 30 inches in floor height must meet the zoning setback. The deck is over 30 inches in floor height (it is located above a patio that is accessed from a daylight basement). The applicant seeks to replace the existing deck with a new deck on the same footprint, put a roof over it and add a wall along the west side (as depicted in Exhibit PD-4, pages 12 and 13). This constitutes the expansion of a nonconforming structure, in that adding the roof and wall to the nonconforming deck would add building height and mass to the deck area and create an additional projection of the roof eave into the setback.

PUBLIC COMMENTS

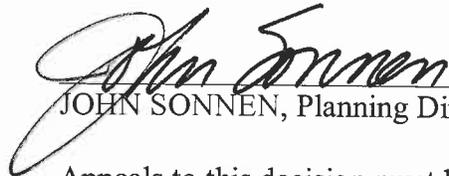
No public comments have been received.

RECOMMENDATION

Based on findings contained in the applicant's submittal in the City record, staff finds that there are sufficient grounds to **approve** this application (MISC-09-11) subject to the following conditions of approval:

1. The expansion of the nonconforming structure shall conform to the drawings contained in Exhibit PD-4 on pages 12, 13, 19 and 21.
2. The eaves of the proposed new section of roof spanning the deck shall maintain a minimum 3 foot setback from the property line, consistent with CDC Section 38.060(B).
3. This approval shall expire 3 years from the effective date of this decision. .

I declare to have no interest in the outcome of this decision due to some past or present involvement with the applicant, the subject property, or surrounding properties, and therefore, can render an impartial decision. The provisions of the Community Development Code Chapter 99 have been met.



 JOHN SONNEN, Planning Director

9/18/2009

 DATE

Appeals to this decision must be filed with the West Linn Planning Department within 14 days of mailing date. Cost is \$2500. The appeal must be filed by an individual who has established standing by submitting written comments prior to or on September 18, 2009. Approval will lapse 3 years from effective approval date unless an extension is obtained.

Mailed this 21 day of September, 2009.
Therefore, the 14-day appeal period ends at 5 p.m., on

October 5, 2009.

ADDENDUM

APPROVAL CRITERIA AND FINDINGS

MIS-09-11

Staff recommends adoption of the findings for approval contained within the applicant's submittal, with the following exceptions and additions:

66.080 ENLARGEMENT OR ALTERATION TO A NONCONFORMING STRUCTURE: PROCESS AND APPROVAL STANDARDS

A. An enlargement or alteration to a nonconforming structure containing a nonconforming use may be permitted subject to review and approval by the Planning Commission under the provisions of Section 99.060(B) and Sections 65.120 through 65.140.

B. An enlargement or alteration to a nonconforming structure containing a conforming use may be permitted subject to the following:

1. If the enlargement, in and of itself, meets all provisions of this Code, the enlargement will be permitted. This exception does not preclude design review or other applicable provisions of this Code. (ORD. 1192)

2. If the enlargement, in and of itself, does not meet all provisions of the Code, review and approval by the Planning Director for single-family structures, and by the Planning Commission for non-single-family structures under the provisions of Section 99.060(B) is required subject to the following standards. (ORD. 1192)

a. The enlargement or alteration will not change the nonconformity; and

b. All other applicable ordinance provisions will be met.

FINDING NO. 1:

The requested enlargement of the deck located at 2155 5th Avenue does not meet all the provisions of the code. Like the deck it replaces, it breaches the 7.5 foot setback from the west property line. However, the requested enlargement will not change the nonconformity because the requested new deck will not extend closer to the west property line than the deck it replaces. The new roof over the deck would project further into the setback than the deck

would, but that is allowed per CDC Section 38.060(B). Therefore, staff concludes that this proposal does not worsen the nonconformity since the roof line and wall line of the least nonconforming portion of the house, located 5 feet from the property line, are proposed to be extended, not the roof lines or wall lines located 1 to 3 feet from the property line. By adding a wall with a small window along the deck frontage that previously contained no wall or screening, the applicant alleviates some of the privacy issues that can arise due to houses being closer to the property line than allowed by the zoning, despite that new building mass is being added. All other applicable CDC provisions will be met, as long as the eaves of the new roof area above the deck do not come within 3 feet of the property line, in keeping with CDC 38.060(B) which requires a 3 foot setback for eaves. Condition of Approval 2 requires the eaves be no less than 3 feet from the property line. The criteria for expanding a nonconforming structure are met.

EXHIBITS

PD-1	AFFADAVIT OF NOTICE.....	5
PD-2	NOTICE MAILING PACKET.....	6-8
PD-3	COMPLETENESS LETTER.....	9
PD-4	APPLICANT'S RESUBMITTAL.....	10-38

AFFIDAVIT OF NOTICE

We, the undersigned do hereby certify that, in the interest of the party (parties) initiating a proposed land use, the following took place on the dates indicated below:

GENERAL

File No. MISC-09-11 Applicant's Name Richard Anyon
Development Name Nonconforming Use - 2155 5th Ave
Scheduled Meeting/Decision Date 9/13/09

NOTICE: Notices were sent at least 20 days prior to the scheduled hearing, meeting, or decision date per Section 99.080 of the Community Development Code. (check below)

TYPE A _____

- A. The applicant (date) _____ (signed) _____
- B. Affected property owners (date) _____ (signed) _____
- C. School District/Board (date) _____ (signed) _____
- D. Other affected gov't. agencies (date) _____ (signed) _____
- E. Affected neighborhood assns. (date) _____ (signed) _____
- F. All parties to an appeal or review (date) _____ (signed) _____

At least 10 days prior to the scheduled hearing or meeting, notice was published/posted:

Tidings (published date) _____ (signed) _____
City's website (posted date) _____ (signed) _____

SIGN

At least 10 days prior to the scheduled hearing, meeting or decision date, a sign was posted on the property per Section 99.080 of the Community Development Code.

(date) _____ (signed) _____

NOTICE: Notices were sent at least 14 days prior to the scheduled hearing, meeting, or decision date per Section 99.080 of the Community Development Code. (check below)

TYPE B

- A. The applicant (date) 9/3/08 (signed) WJ
- B. Affected property owners (date) 9/3/09 (signed) WJ
- C. School District/Board (date) _____ (signed) _____
- D. Other affected gov't. agencies (date) _____ (signed) l
- E. Affected neighborhood assns. (date) 9/3/09 (signed) WJ
Willamette & all

Notice was posted on the City's website at least 10 days prior to the scheduled hearing or meeting.
Date: 9/2/09 (signed) [Signature]

STAFF REPORT mailed to applicant, City Council/Planning Commission and any other applicable parties 10 days prior to the scheduled hearing.

(date) _____ (signed) _____

FINAL DECISION notice mailed to applicant, all other parties with standing, and, if zone change, the County surveyor's office.

(date) _____ (signed) _____

**CITY OF WEST LINN
PLANNING DIRECTOR DECISION**

FILE NO. MIS-09-11

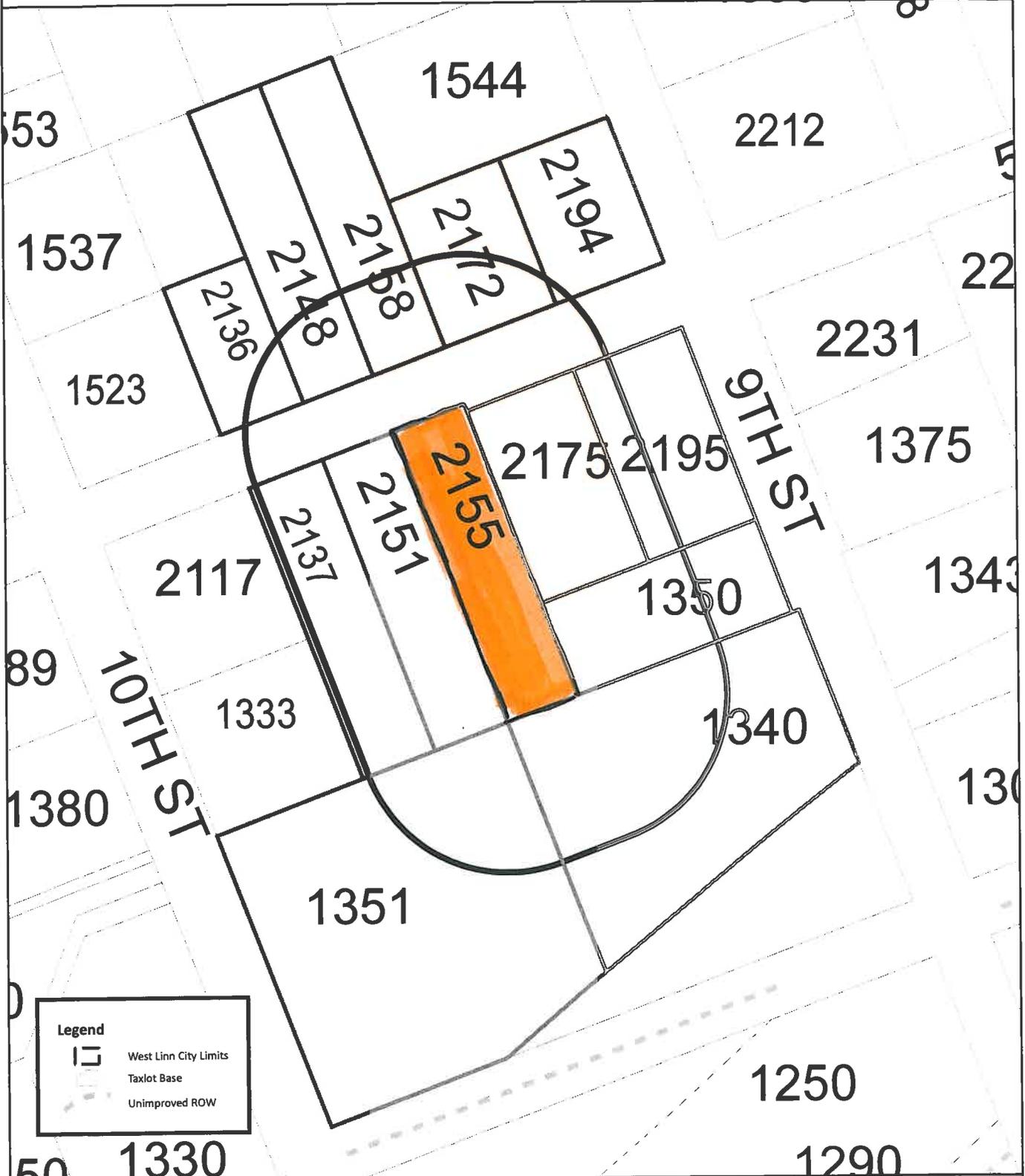
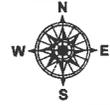
The West Linn Planning Director is considering the request of Richard Ahyou for a permit to enlarge/alter a non-conforming structure by replacing an existing unroofed, unwalled deck with a new deck on the same footprint that has a roof and a west wall. The site is located at 2155 5th Avenue. The permit is needed because the existing and proposed deck, as well as sections of the house, are within 7.5 feet of the property's west property line in the R-10 zone. The decision will be based on the approval criteria in Chapter 66 of the Community Development Code (CDC). The approval criteria from the Community Development Code (Zoning Code) are available for review at City Hall, at the City Library, and on the Planning Department's page of the City's website under Documents/CDC.

You have been notified because County records show you own property within 100 feet of the site located at Tax Lot 5700, Clackamas County Assessor's Map 3-1E-02AB.

All relevant materials in the above noted file are available for inspection at no cost, or copies may be obtained for a minimal charge per page. Although there is no public hearing, your comments and ideas can definitely influence the final decision of the Planning Director. Planning staff looks forward to discussing the application with you. **The final decision is expected to be made on, and no earlier than, September 18, 2009**, so please get in touch with us prior to this date. For further information, please contact Tom Soppe, Associate Planner, at City Hall, 22500 Salamo Rd., West Linn, OR 97068, telephone (503) 742-8660, or e-mail to tsoppe@westlinnoregon.gov

Any appeals to this decision must be filed within 14 days of the final decision date with the Planning Department. Failure to raise an issue in person or by letter, or failure to provide sufficient specificity to afford the decision-maker an opportunity to respond to the issue, precludes the raising of the issue at a subsequent time on appeal or before the Land Use Board of Appeals.

MISC-09-11 2155 5TH AVE



Legend

- West Linn City Limits
- Taxlot Base
- Unimproved ROW

This product is for informational purposes and may not have been prepared for, or be suitable for legal, engineering, or surveying purposes. Users of this information should review or consult the primary data and information sources to ascertain the usability of the information.

Taxlot Base Source: Metro RLIS

NOT TO SCALE



SNAPNOTIFY.MXD / AHA APP 6-16-09

User Name: T Zak
Map Creation Date: Sep 02, 2009

AHYOU RICHARD F & EMILY
CREER
2155 5TH AVE
WEST LINN, OR 97068

BAILEY AMY E & ROB
2194 5TH AVE
WEST LINN, OR 97068

DAVIS DIRK T
1810 RADCLIFFE CT
WEST LINN, OR 97068

DENNIS GARY ALLEN
2148 5TH AVE
WEST LINN, OR 97068

DUNNINGTON LIZABETH T
2136 5TH AVE
WEST LINN, OR 97068

LOONEY TRISHA
2114 SE HEMLOCK ST
PORTLAND, OR 97214

PATTERSON DEVIN L
2175 5TH AVE
WEST LINN, OR 97068

REDMAN GORDON ARTHUR
& LEANNA
1340 9TH ST
WEST LINN, OR 97068

SERGEANT STEVEN C
PO BOX 1631
LAKE OSWEGO, OR 97035

SHADBEH ALI & POURAN
1760 SW 87TH
PORTLAND, OR 97225

STREIKER SCOTT M &
PHYLLIS L
645 GREENLAWN AVE
DAYTON, OH 45403

SUMPTER JERRY R SR &
LORI L
2158 SE 5TH AVE
WEST LINN, OR 97068

WHITNEY ROGER H
2195 5TH AVE
WEST LINN, OR 97068

TODD LARIOS
4804 NE 7TH AVE
PORTLAND, OR 97211

ALL NA



CITY OF
West Linn

MAILED

9/2/09

August 31, 2009

Richard Ahyou
2155 5th Avenue
West Linn, OR 97068

SUBJECT: DR-08-02

Dear Mr. Ahyou:

The Planning Department has declared your application for an expansion/enlargement of a non-conforming structure **complete** on August 31, 2009. Pursuant to Oregon Revised Statutes Chapter 227.178, the city is obliged to exhaust all local review in the next 120 days (by December 29, 2009), including any potential appeal of the director's decision to the West Linn City Council.

A public notice describing your proposal will be mailed to property owners within 100 feet of the site, allowing for a 14-day comment period. The Planning Director will then issue an administrative decision on your application after the comment period is over. You will also receive a copy of the notice, which will inform you of when the end of the comment period will occur.

Please contact me at 503-742-8660, or by email at tsoppe@ci.west-linn.or.us if you have any questions or comments, or if you wish to meet with planning staff regarding these issues.

Sincerely,

Tom Soppe
Associate Planner

c: Todd Larios, 4804 NE 7th Ave., Portland, OR 97211

p:/devrvw/completeness check/compl-MIS-09-11



FILE NO.: MISC-09-11

REQUEST: PERMIT TO ENLARGE/ALTER A NON-
CONFORMING STRUCTURE, FOR NEW
REPLACEMENT DECK WITH ROOF AND WALL, AT
2155 5TH AVENUE

APPLICANTS SUBMITTAL

August 27, 2009
City of West Linn

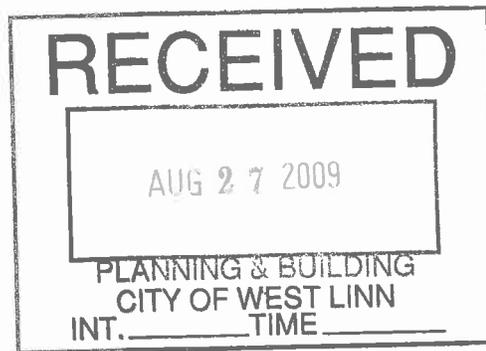
Dear Recipient,

I have met with Tom Soppe with the City of West Linn for a Pre-Application meeting regarding the proposed changes and additions to Richard Ahyous Deck. We realize that the current deck does not meet current set back codes. Also we have learned that parts of the house are even closer to the property lines. We propose to rebuild the current deck making it stronger and visually more appealing. The proposed addition to the deck, is to extend the roof of the house over the deck. Building a new deck and extending the roof would not bring the house closer to conforming to the current codes, but would also not put the house or deck further into non-compliance. The finished deck and roof would remain at the same distance from the property line as the current deck and house are.

Thank you for your consideration.

Todd Larios *TAL Larios* *AUG 27, 09*

General Contractor





West Linn

DEVELOPMENT REVIEW APPLICATION

B

MI-09-11

TYPE OF REVIEW (Please check all boxes that apply):

- | | | | |
|--------------------------|--|-------------------------------------|--|
| <input type="checkbox"/> | Annexation | <input checked="" type="checkbox"/> | Non-Conforming Lots, Uses & Structures |
| <input type="checkbox"/> | Appeal and Review * | <input type="checkbox"/> | One-Year Extension * |
| <input type="checkbox"/> | Conditional Use | <input type="checkbox"/> | Planned Unit Development |
| <input type="checkbox"/> | Design Review | <input type="checkbox"/> | Pre-Application Meeting * |
| <input type="checkbox"/> | Easement Vacation | <input type="checkbox"/> | Quasi-Judicial Plan or Zone Change |
| <input type="checkbox"/> | Extraterritorial Ext. of Utilities | <input type="checkbox"/> | Street Vacation |
| <input type="checkbox"/> | Final Plat or Plan | <input type="checkbox"/> | Subdivision |
| <input type="checkbox"/> | Flood Plain Construction | <input type="checkbox"/> | Temporary Uses * |
| <input type="checkbox"/> | Hillside Protection and Erosion Control | <input type="checkbox"/> | Tualatin River Greenway |
| <input type="checkbox"/> | Historic District Review | <input type="checkbox"/> | Variance |
| <input type="checkbox"/> | Legislative Plan or Change | <input type="checkbox"/> | Water Resource Area Protection/Wetland |
| <input type="checkbox"/> | Lot Line Adjustment * /** | <input type="checkbox"/> | Willamette River Greenway |
| <input type="checkbox"/> | Minor Partition (Preliminary Plat or Plan) | <input type="checkbox"/> | Other/Misc |

Home Occupation / Pre-Application / Sidewalk Use Application * / Permanent Sign Review * / Temporary Sign Application require individual application forms available in the forms and application section of the City Website or at City Hall.

TOTAL FEES/DEPOSIT _____ * No CD required/** Only one copy needed

Richard AHYOU 2155 5th Ave West Linn 97068

OWNER'S	ADDRESS	CITY	ZIP	PHONE(res.& bus.)
Todd LARIOS	4804 Ne 7th Ave	Portland	OR	503-888-9419

APPLICANT'S	ADDRESS	CITY	ZIP	PHONE(res.& bus.)

CONSULTANT	ADDRESS	CITY	ZIP	PHONE

SITE LOCATION 2155 5th Ave West Linn 97068

Assessor's Map No.: _____ Tax Lot(s): _____ Total Land Area: _____

- All application fees are non-refundable (excluding deposit).
- The owner/applicant or their representative should be present at all public hearings.
- A denial or grant may be reversed on appeal. No permit will be in effect until the appeal period has expired.

4. **Four (4) complete hard-copy sets (single sided) of application materials must be submitted with this application. One (1) complete set of digital application materials must also be submitted on CD in PDF format.**

The undersigned property owner(s) hereby authorizes the filing of this application, and authorizes on site review by authorized staff. I hereby agree to comply with all code requirements applicable to my application.

SIGNATURE OF PROPERTY OWNER(S)

X Richard Ayou Date Aug 5 09

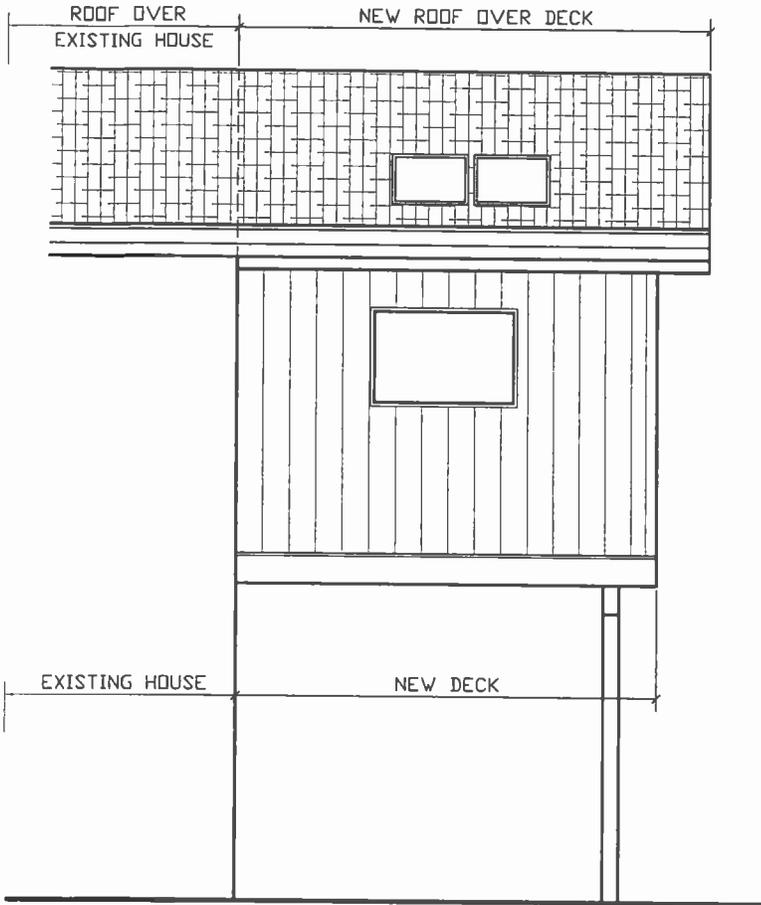
SIGNATURE OF APPLICANT(S)

X Todd Larios Date Aug 25, 09

BY SIGNING THIS APPLICATION, THE CITY IS AUTHORIZED REASONABLE ACCESS TO THE PROPERTY. ACCEPTANCE OF THIS APPLICATION DOES NOT INFER A COMPLETE SUBMITTAL. COMPLETENESS WILL BE DETERMINED WITHIN 30 DAYS OF SUBMITTAL.

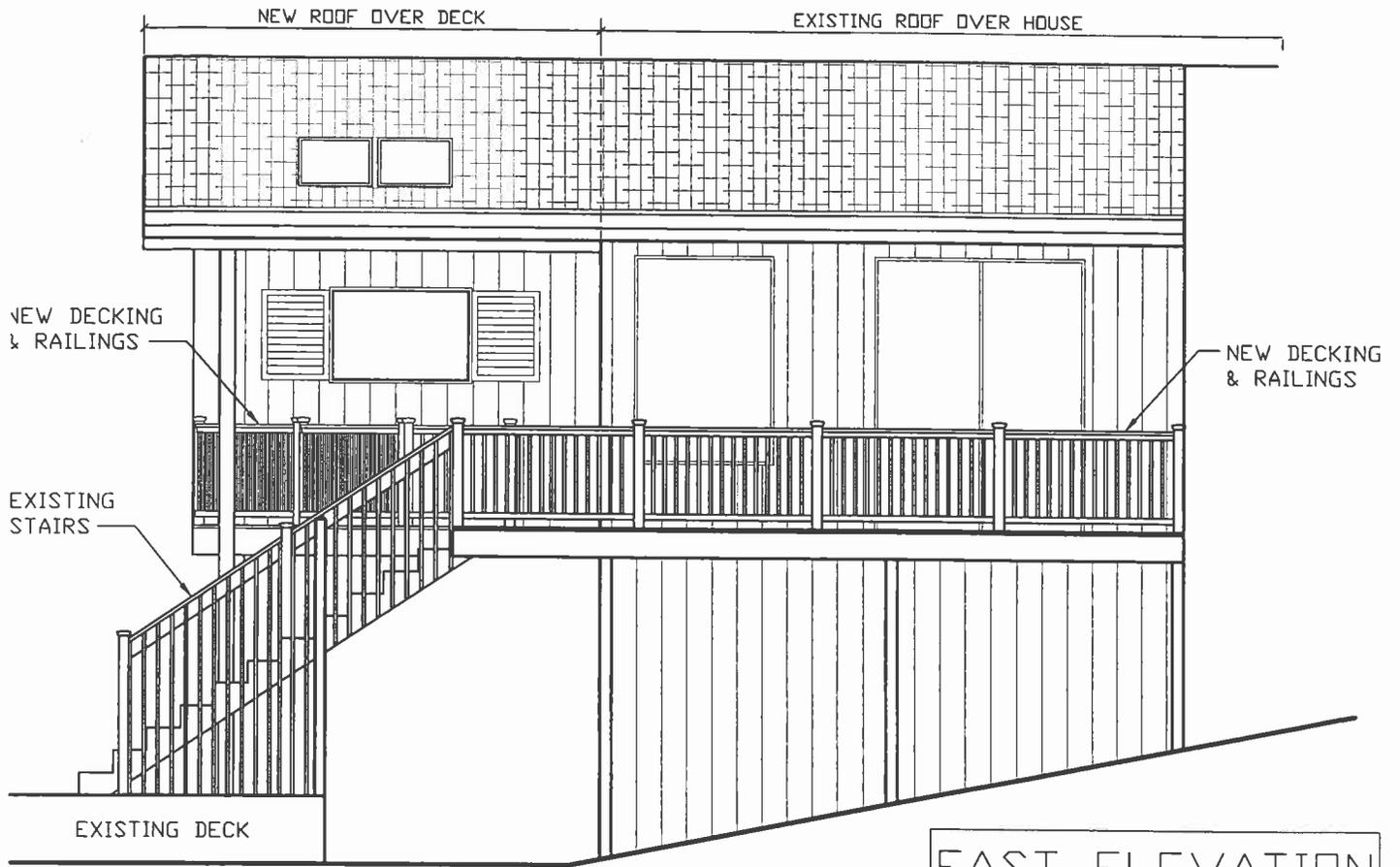
||

PLANNING AND BUILDING; 22500 SALAMO RD #1000; WEST LINN, OR 97068; PHONE: 656-4211 FAX: 656-4106



WEST ELEVATION
 SCALE: 1/4" = 1'-0"

2155 5TH AVE
 WEST LINN, OR 97068



EAST ELEVATION
SCALE: 1/4" = 1'-0"

2155 5TH AVE
WEST LINN, OR 97068





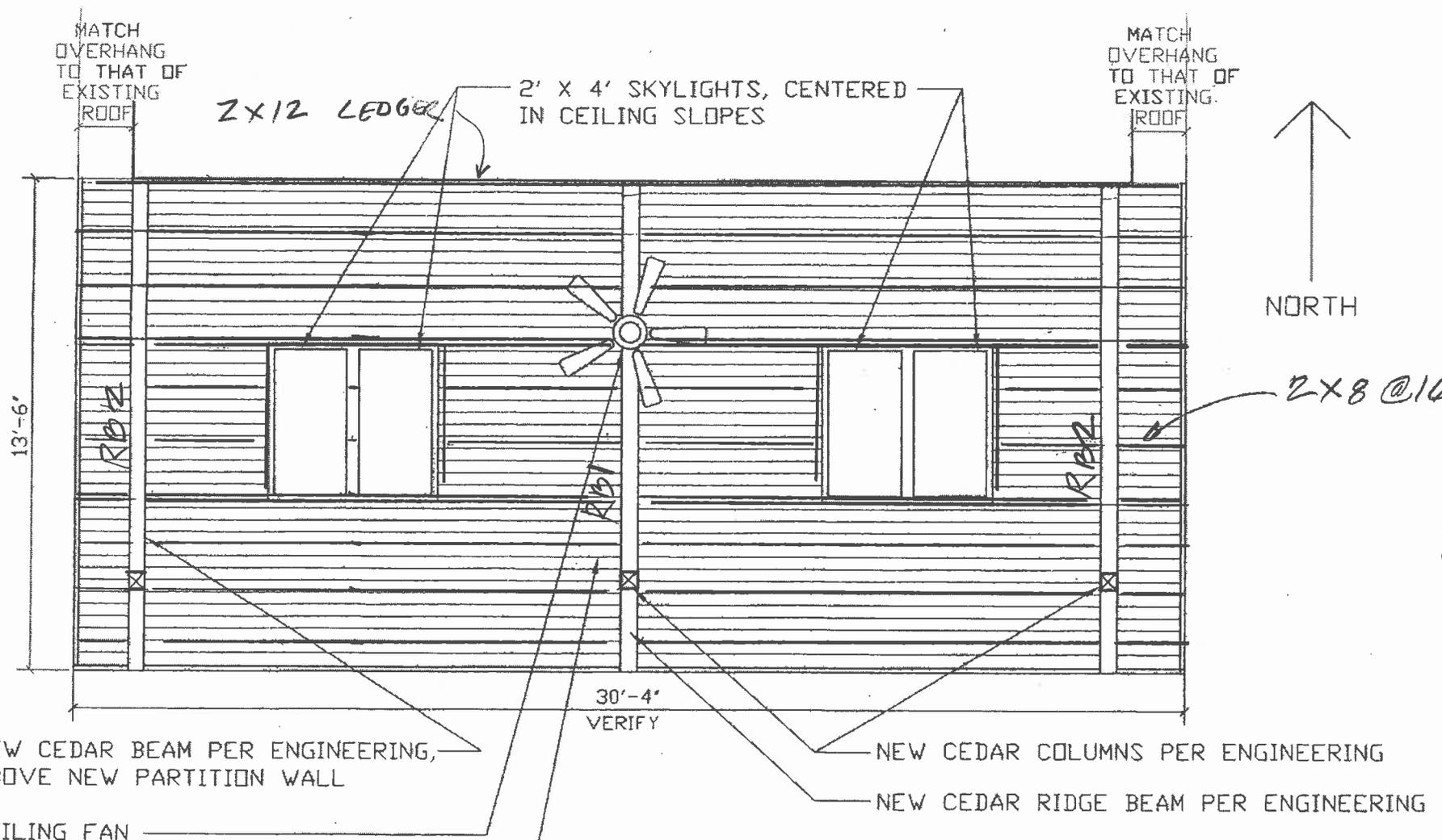
161



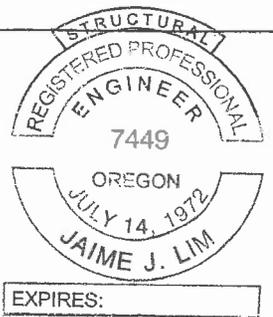


18





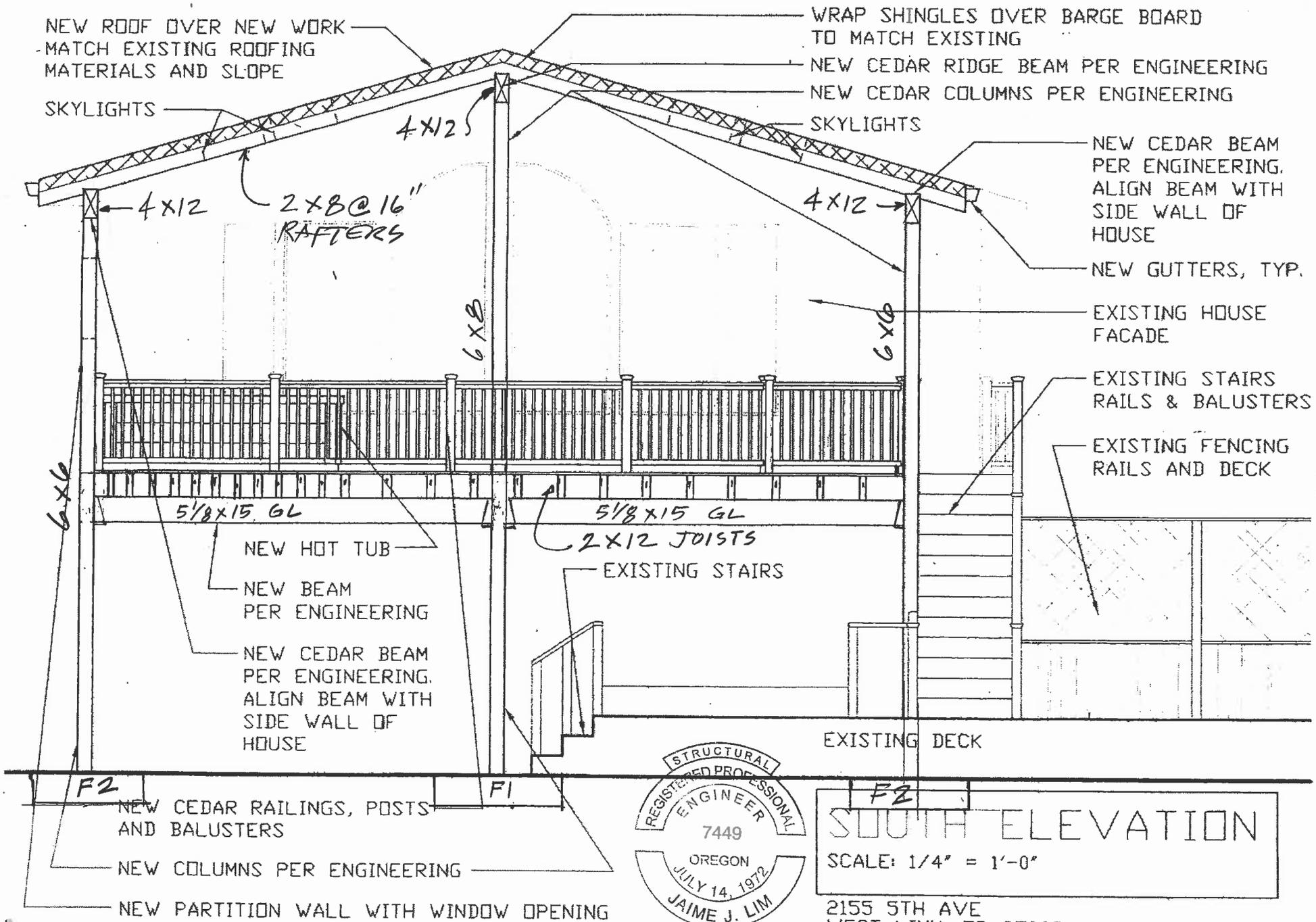
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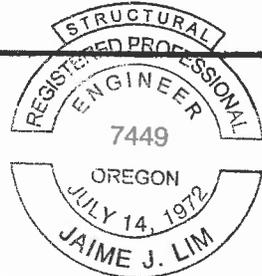
REFLECTED CEILING PLAN
 SCALE: 1/4" = 1'-0"

2155 5TH AVE
 WEST LINN, OR 97068

W



21



SOUTH ELEVATION
 SCALE: 1/4" = 1'-0"

2155 5TH AVE
 WEST LINN, OR 97068

EXPIRES:

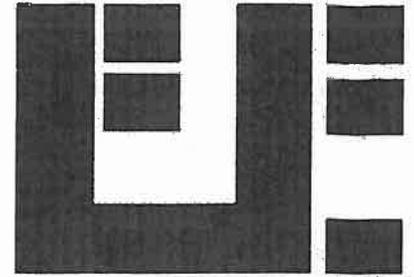
A

UNITED ENGINEERING, INC.

Consulting Engineering * Civil * Structural * Environmental Engineering * Planning

922 N. Killingsworth St. - Suite: 1A
 Portland, OR 97217, USA
 Email : jaimelim@asianreporter.com

Telephone : (503) 289-7775
 Fax : (503) 283-4445

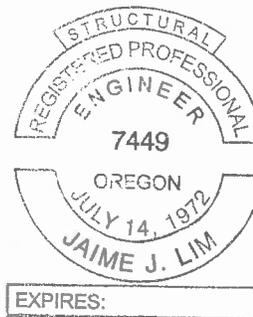


BEAM SCHEDULE

MARK	SIZE	END CONNECTION
B1	5/8x15 GLULAM	HU 5.25/16
B2	5/8x15 GLULAM	HU 5.25/16
B3	4x12	HU 4x12
B4	4x12	HU 4x12
RB1	4x12	HU 4x12
RB2	4x12	HU 4x12
JST 1	2x12	@ 16" o/c
JST 2	2x12	@ 8" o/c

FOOTING SCHEDULE

MARK	SIZE	REINFORCING
F1	48" x 48" x 12"	#4 @ 7" EW
F2	36" x 36" x 12"	#4 @ 6" EW



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Consulting Engineering * Civil * Structural * Environmental Engineering * Planning

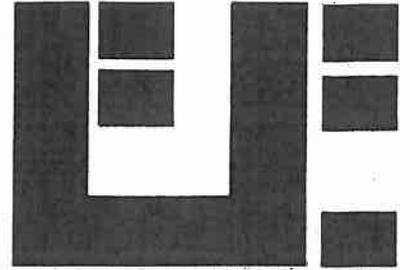
922 N. Killingsworth St. - Suite: 1A

Portland, OR 97217 USA

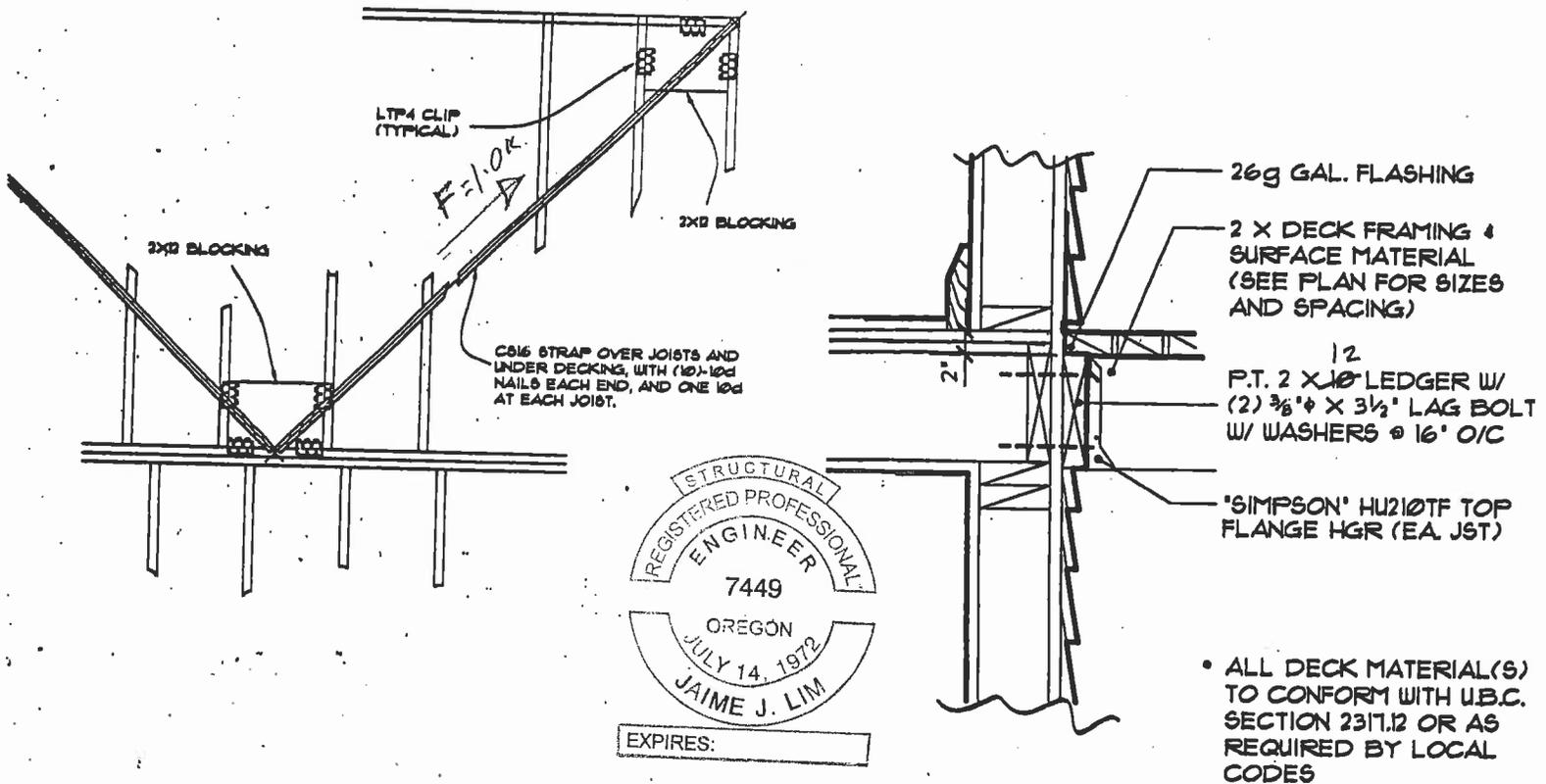
Email : jaimelim@asianreporter.com

Telephone : (503) 289-7775

Fax : (503) 283-4445



RICHARD AAYOU



① PLAN VIEW OF DECK BRACING

② DECK LEDGER
3/4" = 1'-0"

SEISMIC

$$DEAD \text{ LOAD} = 10 \text{ PSF} \times 13' \times 27' = 3510 \# + 12,000 \text{ K}$$

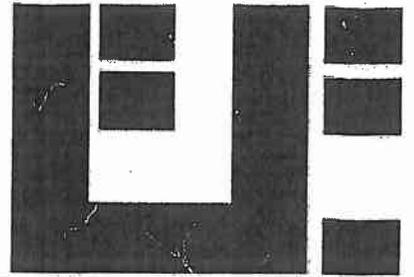
$$SEISMIC \text{ BASE SHEAR } V = .20 (3510 + 12000) = 15.5 \text{ K}$$

$$BRACING \text{ F} = \sqrt{2} (15.5 \text{ K}) = 3.1 \text{ K}$$

USE SIMPSON CS16 STRAP BRACING (2 SETS)

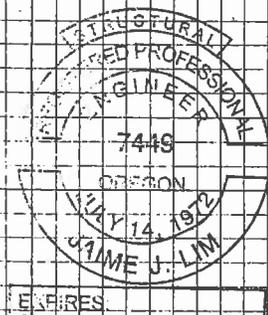
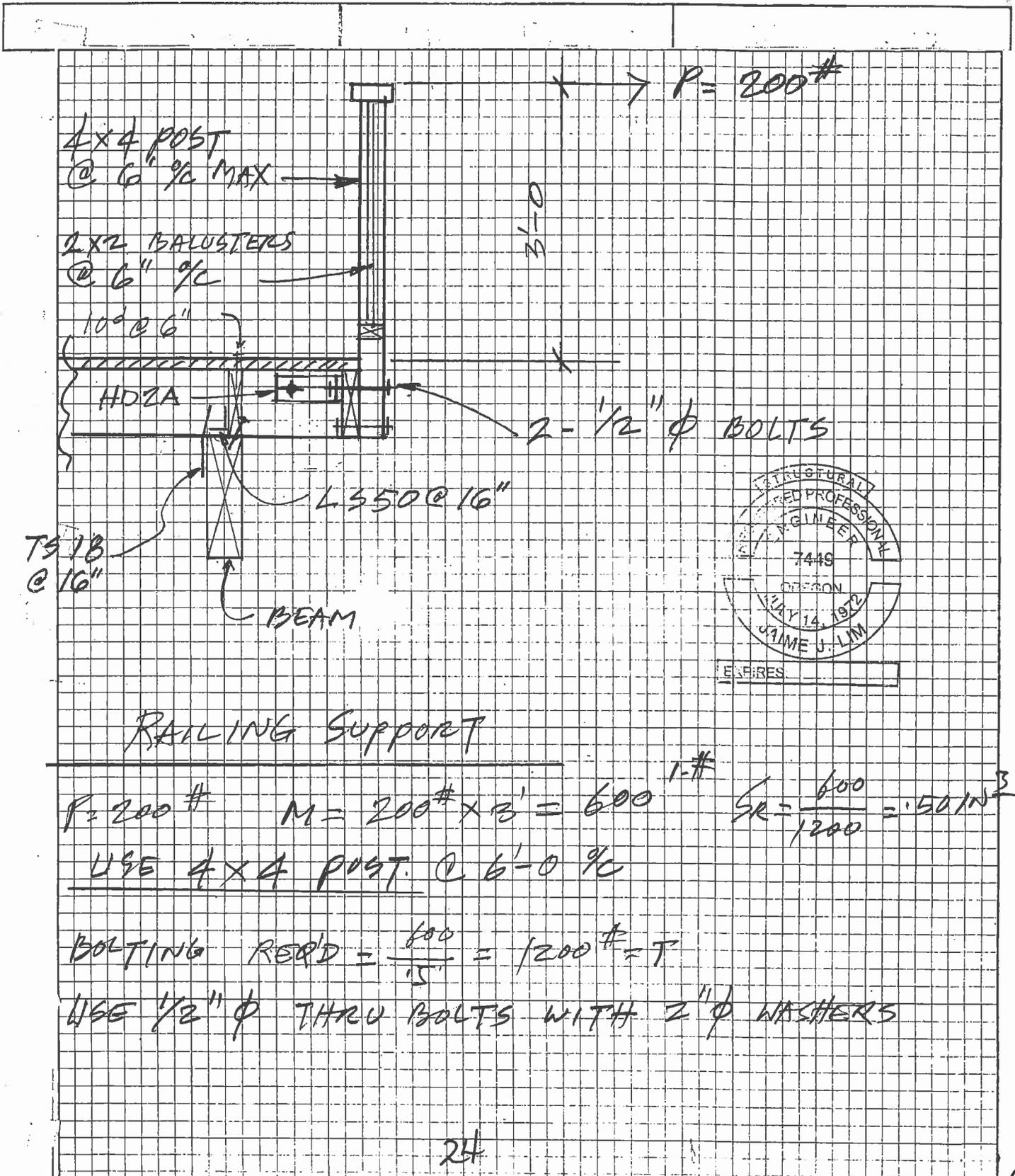
UNITED ENGINEERING, INC.

Consulting Engineering * Civil * Structural * Environmental Engineering * Planning



922 N. Killingsworth St. - Suite: 1A
 Portland, OR 97217 USA
 Email : jaimelim@asianreporter.com

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 Fax : (503) 283-4445



RAILING SUPPORT

$P = 200 \#$ $M = 200 \# \times 3' = 600 \text{ ft}\cdot\#$ $S_R = \frac{600}{1200} = .50 \text{ IN}^3$

USE 4x4 POST @ 6'-0" o/c

BOLTING REQ'D = $\frac{600}{.5} = 1200 \# = T$

USE 1/2" φ THRU BOLTS WITH 2" φ WASHERS

UNITED ENGINEERING, INC.

Consulting Engineering * Civil * Structural * Environmental Engineering * Planning

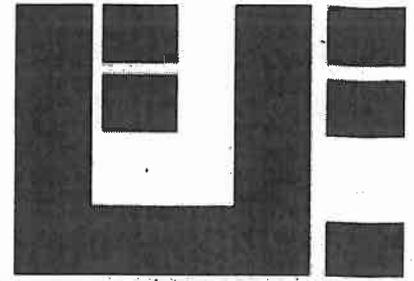
922 N. Killingsworth St. - Suite: 1A

Portland, OR 97217 USA

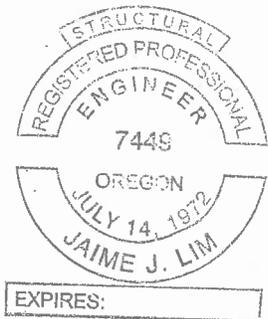
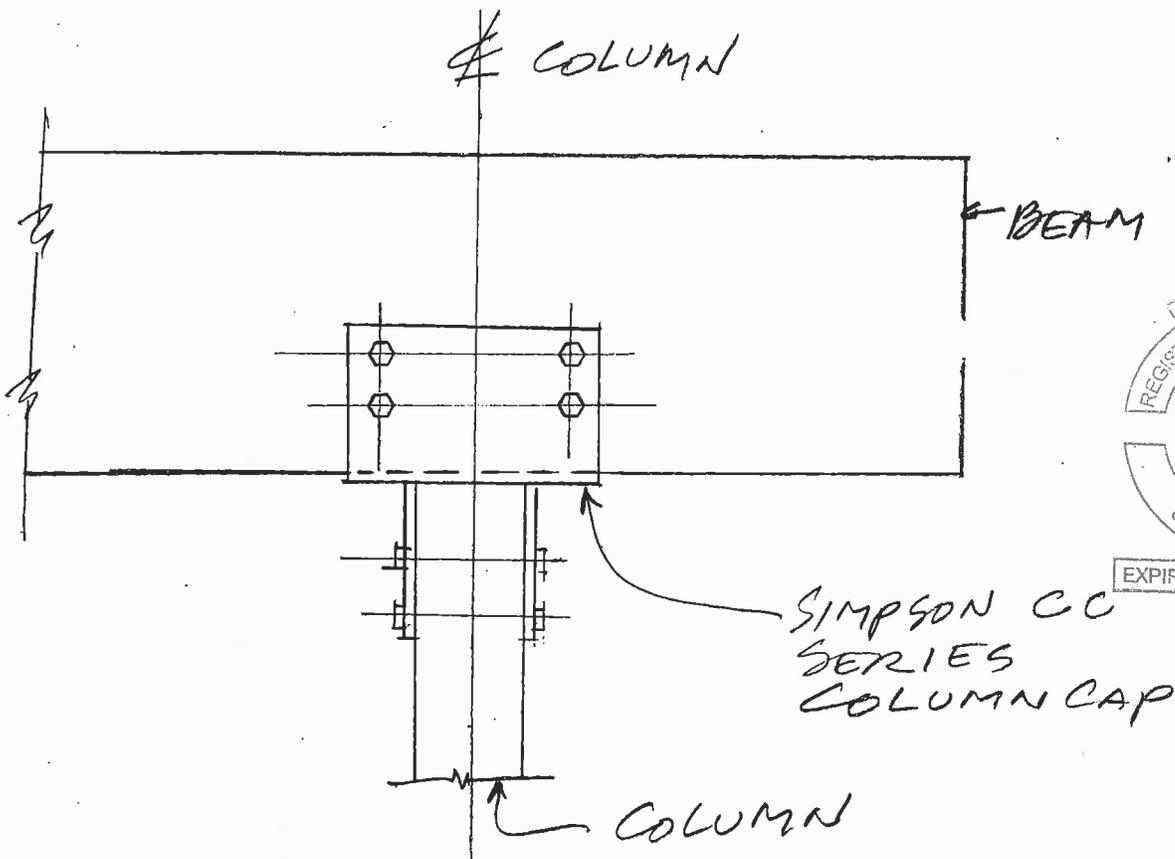
Email : jaimelim@asianreporter.com

Telephone : (503) 289-7775

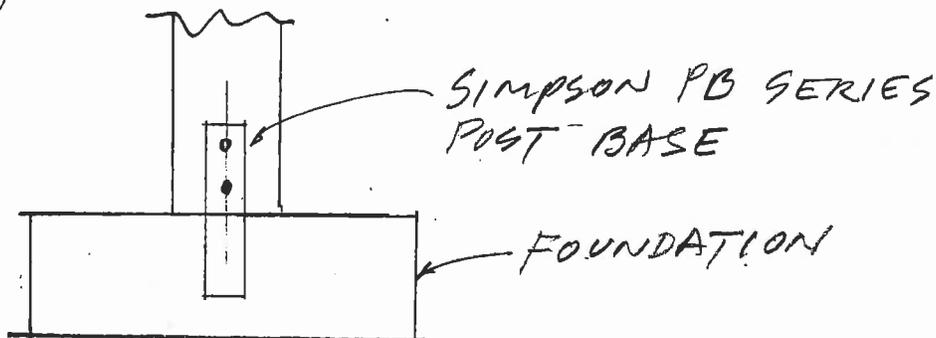
Fax : (503) 283-4445



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(X) BEAM COLUMN DETAIL



Project: Richard Ahyou
 Location: Floor Beam B1
 Uniformly Loaded Floor Beam
 [2006 International Building Code(2005 NDS)]
 5.125 IN x 15.0 IN x 13.5 FT
 24F-E4 - E-Rated Western Species - Dry Use
 Section Adequate By: 0.1%
 Controlling Factor: Moment



Jaime Lim, P.E.
 First United Engineering
 922 N. Killingsworth St.
 Portland, Oregon 97217

page
 of

StruCalc Version 8.0.98.0

7/24/2009 9:30:40 AM

DEFLECTIONS		Center
Live Load	0.00	IN L/MAX
Dead Load	0.44	in
Total Load	0.44	IN L/371
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

REACTIONS		A	B
Live Load	0	lb	0 lb
Dead Load	10237	lb	10237 lb
Total Load	10237	lb	10237 lb
Bearing Length	3.07	in	3.07 in

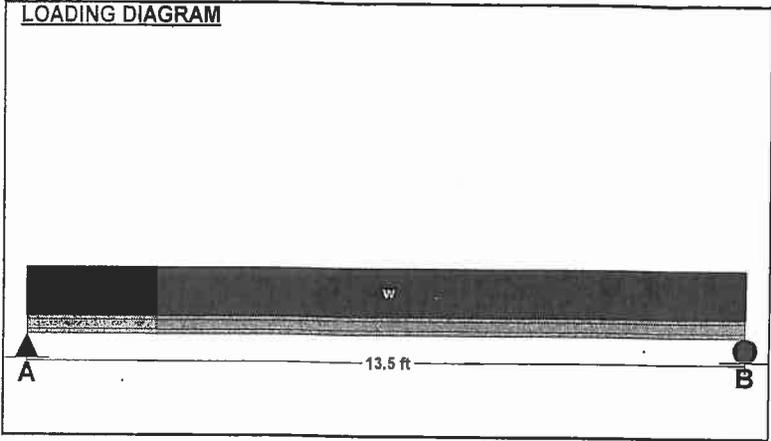
BEAM DATA		Center
Span Length	13.5	ft
Unbraced Length-Top	0	ft
Floor Duration Factor	1.00	
Camber Adj. Factor	1	
Camber Required	0.44	
Notch Depth	0.00	

MATERIAL PROPERTIES			
24F-E4 - E-Rated Western Species			
	Base Values	Adjusted	Controlled by:
Bending Stress:	Fb = 2400 psi	Fb' = 2160 psi	
	Fb_cmpr = 1450 psi		
	Cd=0.90		
Shear Stress:	Fv = 265 psi	Fv' = 239 psi	
	Cd=0.90		
Modulus of Elasticity:	E = 1800 ksi	E' = 1800 ksi	
Min. Mod. of Elasticity:	E_min = 930 ksi	E_min' = 930 ksi	
Comp. ⊥ to Grain:	Fc ⊥ = 650 psi	Fc ⊥' = 650 psi	

Controlling Moment: 34552 ft-lb
 6.75 ft from left support
 Created by dead loads only on all span(s).

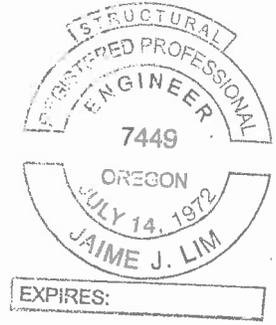
Controlling Shear: 8395 lb
 At a distance d from support.
 Created by dead loads only on all span(s).

Comparisons with required sections:	Req'd	Provided
Section Modulus:	191.95 in3	192.19 in3
Area (Shear):	52.8 in2	76.88 in2
Moment of Inertia (deflection):	932.74 in4	1441.41 in4
Moment:	34552 ft-lb	34594 ft-lb
Shear:	8395 lb	12223 lb



FLOOR LOADING			
		Side 1	Side 2
Floor Live Load	FLL =	40 psf	40 psf
Floor Dead Load	FDL =	15 psf	15 psf
Floor Tributary Width	FTW =	0 ft	0 ft
Wall Load	WALL =	1500 plf	

BEAM LOADING		
Beam Total Live Load:	wL =	0 plf
Beam Total Dead Load:	wD =	1500 plf
Beam Self Weight:	BSW =	17 plf
Total Maximum Load:	wT =	1517 plf



NOTES

Project: Richard Ahyou
 Location: Floor Beam B2
 Uniformly Loaded Floor Beam
 [2006 International Building Code(2005 NDS)]
 5.125 IN x 15.0 IN x 13.5 FT
 24F-E4 - E-Rated Western Species - Dry Use
 Section Adequate By: 134.8%
 Controlling Factor: Moment



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DEFLECTIONS		Center
Live Load	0.00	IN L/MAX
Dead Load	0.19	in
Total Load	0.19	IN L/870
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

REACTIONS		A	B
Live Load	0	lb	0 lb
Dead Load	4365	lb	4365 lb
Total Load	4365	lb	4365 lb
Bearing Length	1.31	in	1.31 in

BEAM DATA		Center
Span Length	13.5	ft
Unbraced Length-Top	0	ft
Floor Duration Factor	1.00	
Camber Adj. Factor	1	
Camber Required	0.19	
Notch Depth	0.00	

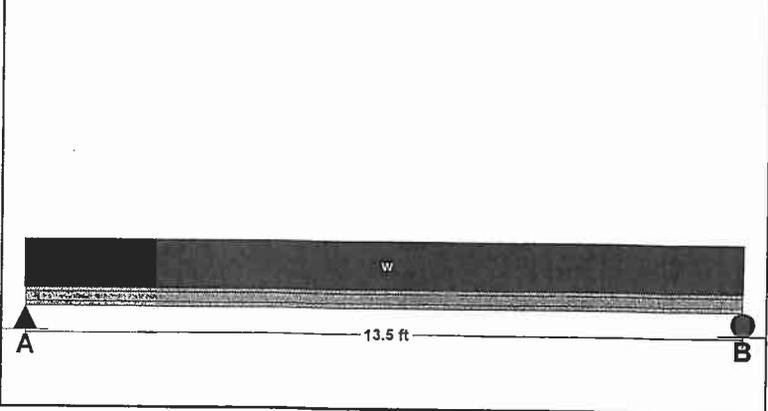
MATERIAL PROPERTIES			
24F-E4 - E-Rated Western Species			
	Base Values	Adjusted	
Bending Stress:	Fb =	2400 psi	Controlled by:
	Fb_cmp =	1450 psi	Fb' =
	Cd=0.90		
Shear Stress:	Fv =	265 psi	Fv' =
	Cd=0.90		
Modulus of Elasticity:	E =	1800 ksi	E' =
Min. Mod. of Elasticity:	E_min =	930 ksi	E_min' =
Comp. \perp to Grain:	Fc \perp =	650 psi	Fc \perp ' =

Controlling Moment: 14732 ft-lb
 6.75 ft from left support
 Created by dead loads only on all span(s).

Controlling Shear: -3579 lb
 At a distance d from support.
 Created by dead loads only on all span(s).

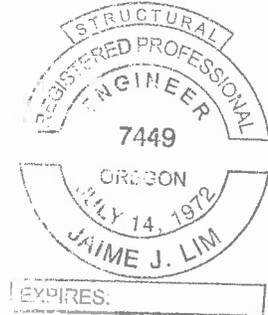
Comparisons with required sections:	Req'd	Provided
Section Modulus:	81.84 in3	192.19 in3
Area (Shear):	22.51 in2	76.88 in2
Moment of Inertia (deflection):	397.7 in4	1441.41 in4
Moment:	14732 ft-lb	34594 ft-lb
Shear:	-3579 lb	12223 lb

LOADING DIAGRAM



FLOOR LOADING			
		Side 1	Side 2
Floor Live Load	FLL =	40 psf	40 psf
Floor Dead Load	FDL =	15 psf	15 psf
Floor Tributary Width	FTW =	0 ft	0 ft
Wall Load	WALL =	630 plf	

BEAM LOADING	
Beam Total Live Load:	wL = 0 plf
Beam Total Dead Load:	wD = 630 plf
Beam Self Weight:	BSW = 17 plf
Total Maximum Load:	wT = 647 plf



NOTES

Project: Richard Ahyou
 Location: Multi-Span Roof Beam RB1
 Multi-Span Roof Beam
 [2006 International Building Code(2005 NDS)]
 3.5 IN x 11.5 IN x 13.5 FT (10 + 3.5)
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 13.3%
 Controlling Factor: Moment



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LOADING DIAGRAM



DEFLECTIONS	Center		Right	
Live Load	0.11	IN L/1082	-0.12	IN L/338
Dead Load	0.05	in	-0.03	in
Total Load	0.16	IN L/750	-0.15	IN L/273
Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180				

REACTIONS	A	B
Live Load	1750 lb	3189 lb
Dead Load	963 lb	2000 lb
Total Load	2713 lb	5189 lb
Bearing Length	1.24 in	2.37 in

BEAM DATA	Center	Right
Span Length	10 ft	3.5 ft
Unbraced Length-Top	0 ft	0 ft
Unbraced Length-Bottom	10 ft	3.5 ft
Roof Pitch	1 :12	
Roof Duration Factor	1.15	
Notch Depth	0.00	

MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

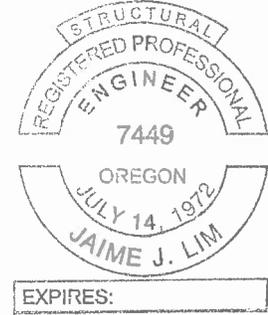
	Base Values	Adjusted
Bending Stress:	Fb = 900 psi Cd=1.15 CF=1.10	Fb' = 1139 psi
Shear Stress:	Fv = 180 psi Cd=1.15	Fv' = 207 psi
Modulus of Elasticity:	E = 1600 ksi	E' = 1600 ksi
Min. Mod. of Elasticity:	E_min = 580 ksi	E_min' = 580 ksi
Comp. ⊥ to Grain:	Fc ⊥ = 625 psi	Fc ⊥' = 625 psi

ROOF LOADING	Center	Right
Roof Live Load	RLL = 25 psf	25 psf
Roof Dead Load	RDL = 15 psf	15 psf
Roof Tributary Width Side One	TW1 = 7 ft	7 ft
Roof Tributary Width Side Two	TW2 = 7 ft	7 ft
Wall Load	WALL = 0 plf	0 plf

BEAM LOADING	Center	Right
Total Live Load	350 plf	350 plf
Total Dead Load (Adjusted for Roof Pitch)	211 plf	211 plf
Beam Self Weight	9 plf	9 plf
Total Load	569 plf	569 plf

Controlling Moment: 6462 ft-lb
 4.8 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2
Controlling Shear: -2684 lb
 At a distance d from right support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2, 3

Comparisons with required sections:	Req'd	Provided
Section Modulus:	68.11 in3	77.15 in3
Area (Shear):	19.45 in2	40.25 in2
Moment of Inertia (deflection):	157.48 in4	443.59 in4
Moment:	6462 ft-lb	7319 ft-lb
Shear:	-2684 lb	5555 lb



NOTES

Project: Richard Ahyou
 Location: Multi-Span Roof Beam RB2
 Multi-Span Roof Beam
 [2006 International Building Code(2005 NDS)]
 3.5 IN x 11.5 IN x 13.5 FT (10 + 3.5)
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 5.9%
 Controlling Factor: Moment



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DEFLECTIONS	Center	Right
Live Load	0.11 IN L/1082	-0.12 IN L/338
Dead Load	0.06 in	-0.06 in
Total Load	0.17 IN L/689	-0.19 IN L/225
Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180		

REACTIONS	A	B
Live Load	1750 lb	2161 lb
Dead Load	1055 lb	1381 lb
Total Load	2805 lb	3542 lb
Bearing Length	1.28 in	1.62 in

BEAM DATA	Center	Right
Span Length	10 ft	3.5 ft
Unbraced Length-Top	0 ft	0 ft
Unbraced Length-Bottom	10 ft	3.5 ft
Roof Pitch	1	:12
Roof Duration Factor	1.15	
Notch Depth	0.00	

MATERIAL PROPERTIES

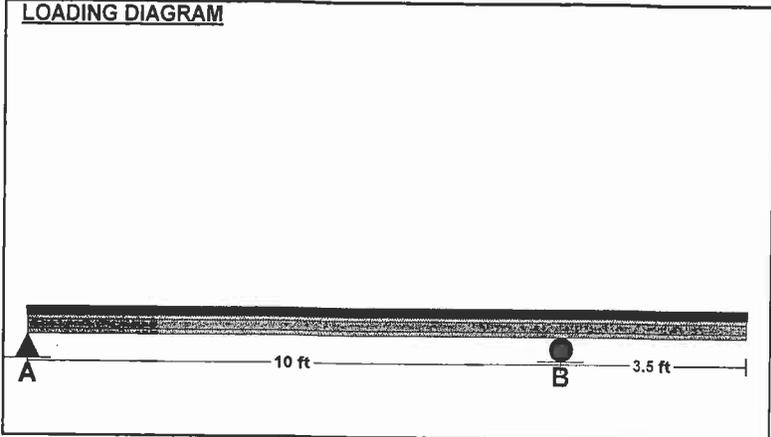
#2 - Douglas-Fir-Larch

	Base Values	Adjusted
Bending Stress:	Fb = 900 psi Cd=1.15 CF=1.10	Fb' = 1139 psi
Shear Stress:	Fv = 180 psi Cd=1.15	Fv' = 207 psi
Modulus of Elasticity:	E = 1600 ksi	E' = 1600 ksi
Min. Mod. of Elasticity:	E_min = 580 ksi	E_min' = 580 ksi
Comp. ⊥ to Grain:	Fc-⊥ = 625 psi	Fc-⊥' = 625 psi

Controlling Moment: 6908 ft-lb
 4.9 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2

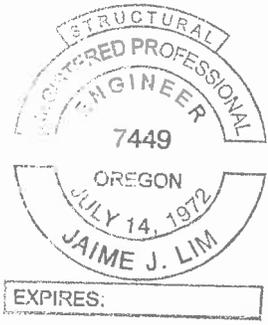
Controlling Shear: -2438 lb
 At a distance d from right support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2, 3

Comparisons with required sections:	Req'd	Provided
Section Modulus:	72.82 in3	77.15 in3
Area (Shear):	17.67 in2	40.25 in2
Moment of Inertia (deflection):	177.78 in4	443.59 in4
Moment:	6908 ft-lb	7319 ft-lb
Shear:	-2438 lb	5555 lb



ROOF LOADING	Center	Right
Roof Live Load	RLL = 25 psf	25 psf
Roof Dead Load	RDL = 15 psf	15 psf
Roof Tributary Width Side One	TW1 = 7 ft	2 ft
Roof Tributary Width Side Two	TW2 = 7 ft	2 ft
Wall Load	WALL = 0 plf	0 plf

BEAM LOADING	Center	Right
Total Live Load	350 plf	100 plf
Total Dead Load (Adjusted for Roof Pitch)	211 plf	60 plf
Beam Self Weight	9 plf	9 plf
Total Load	569 plf	169 plf



NOTES

Project: Richard Ahyou
 Location: Column 1
 Column
 [2006 International Building Code(2005 NDS)]
 5.5 IN x 5.5 IN x 8.0 FT
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 16.4%



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VERTICAL REACTIONS

Live Load: Vert-LL-Rxn = 10000 lb
 Dead Load: Vert-DL-Rxn = 5052 lb
 Total Load: Vert-TL-Rxn = 15052 lb

COLUMN DATA

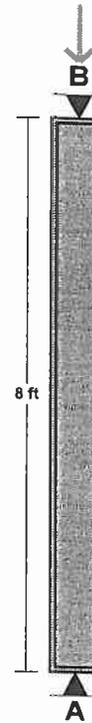
Total Column Length: 8 ft
 Unbraced Length (X-Axis) Ly: 8 ft
 Unbraced Length (Y-Axis) Ly: 8 ft
 Column End Condition-K (e): 1
 Axial Load Duration Factor 1.00

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

	<u>Base Values</u>	<u>Adjusted</u>
Compressive Stress:	Fc = 700 psi Cd=1.00 Cp=0.85	Fc' = 595 psi
Bending Stress (X-X Axis):	Fbx = 750 psi Cd=1.00 CF=1.00	Fbx' = 750 psi
Bending Stress (Y-Y Axis):	Fby = 750 psi Cd=1.00 CF=1.00	Fby' = 750 psi
Modulus of Elasticity:	E = 1300 ksi	E' = 1300 ksi
Min. Mod. of Elasticity:	E_min = 470 ksi	E_min' = 470 ksi
Column Section (X-X Axis):	dx = 5.5 in	
Column Section (Y-Y Axis):	dy = 5.5 in	
Area:	A = 30.25 in ²	
Section Modulus (X-X Axis):	Sx = 27.73 in ³	
Section Modulus (Y-Y Axis):	Sy = 27.73 in ³	
Slenderness Ratio:	L _{ex} /dx = 17.45 L _{ey} /dy = 17.45	

LOADING DIAGRAM



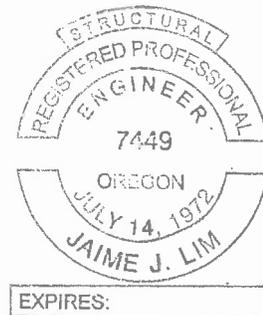
AXIAL LOADING

Live Load: PL = 10000 lb
 Dead Load: PD = 5000 lb
 Column Self Weight: CSW = 52 lb
 Total Load: PT = 15052 lb

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D)
 Actual Compressive Stress: Fc = 498 psi
 Allowable Compressive Stress: Fc' = 595 psi
 Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb
 Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb
 Moment Due to Lateral Loads (X-X Axis): Mx = 0 ft-lb
 Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb
 Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi
 Allowable Bending Stress (X-X Axis): Fbx' = 750 psi
 Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi
 Allowable Bending Stress (Y-Y Axis): Fby' = 750 psi
 Combined Stress Factor: CSF = 0.84

NOTES



EXPIRES:

Project: Richard Ahyou
 Location: Column 2
 Column
 [2006 International Building Code(2005 NDS)]
 5.5 IN x 5.5 IN x 8.0 FT
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 10.8%



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VERTICAL REACTIONS

Live Load: Vert-LL-Rxn = 10000 lb
 Dead Load: Vert-DL-Rxn = 6052 lb
 Total Load: Vert-TL-Rxn = 16052 lb

COLUMN DATA

Total Column Length: 8 ft
 Unbraced Length (X-Axis) Ly: 8 ft
 Unbraced Length (Y-Axis) Ly: 8 ft
 Column End Condition-K (e): 1
 Axial Load Duration Factor 1.00

COLUMN PROPERTIES

#2 - Douglas-Fir-Larch

	<u>Base Values</u>	<u>Adjusted</u>
Compressive Stress:	Fc = 700 psi Cd=1.00 Cp=0.85	Fc' = 595 psi
Bending Stress (X-X Axis):	Fbx = 750 psi Cd=1.00 CF=1.00	Fbx' = 750 psi
Bending Stress (Y-Y Axis):	Fby = 750 psi Cd=1.00 CF=1.00	Fby' = 750 psi
Modulus of Elasticity:	E = 1300 ksi	E' = 1300 ksi
Min. Mod. of Elasticity:	E_min = 470 ksi	E_min' = 470 ksi
Column Section (X-X Axis):	dx = 5.5 in	
Column Section (Y-Y Axis):	dy = 5.5 in	
Area:	A = 30.25 in ²	
Section Modulus (X-X Axis):	Sx = 27.73 in ³	
Section Modulus (Y-Y Axis):	Sy = 27.73 in ³	
Slenderness Ratio:	Lex/dx = 17.45 Ley/dy = 17.45	

LOADING DIAGRAM



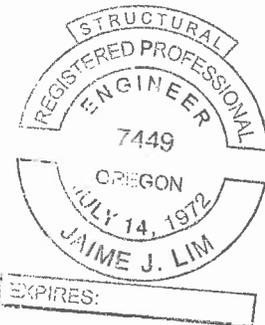
AXIAL LOADING

Live Load: PL = 10000 lb
 Dead Load: PD = 6000 lb
 Column Self Weight: CSW = 52 lb
 Total Load: PT = 16052 lb

Column Calculations (Controlling Case Only):

Controlling Load Case: Axial Total Load Only (L + D)
 Actual Compressive Stress: Fc = 531 psi
 Allowable Compressive Stress: Fc' = 595 psi
 Eccentricity Moment (X-X Axis): Mx-ex = 0 ft-lb
 Eccentricity Moment (Y-Y Axis): My-ey = 0 ft-lb
 Moment Due to Lateral Loads (X-X Axis): Mx = 0 ft-lb
 Moment Due to Lateral Loads (Y-Y Axis): My = 0 ft-lb
 Bending Stress Lateral Loads Only (X-X Axis): Fbx = 0 psi
 Allowable Bending Stress (X-X Axis): Fbx' = 750 psi
 Bending Stress Lateral Loads Only (Y-Y Axis): Fby = 0 psi
 Allowable Bending Stress (Y-Y Axis): Fby' = 750 psi
 Combined Stress Factor: CSF = 0.89

NOTES



Project: Richard Ahyou
 Location: Footing 1
 Footing
 [2006 International Building Code(2005 NDS)]
 Footing Size: 4.0 FT x 4.0 FT x 12.00 IN
 Reinforcement: #4 Bars @ 8.00 IN. O.C. E/W / (6) min.
 Section Footing Design Adequate



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FOOTING PROPERTIES	
Allowable Soil Bearing Pressure:	Qs = 1500 psf
Concrete Compressive Strength:	F'c = 2500 psi
Reinforcing Steel Yield Strength:	Fy = 40000 psi
Concrete Reinforcement Cover:	c = 3 in

FOOTING SIZE	
Width:	W = 4 ft
Length:	L = 4 ft
Depth:	Depth = 12 in
Effective Depth to Top Layer of Steel:	d = 8.25 in

COLUMN AND BASEPLATE SIZE	
Column Type:	Steel
Column Width:	m = 4 in
Column Depth:	n = 4 in
Baseplate Width:	bsw = 6 in
Baseplate Length:	bsl = 6 in

FOOTING CALCULATIONS

Bearing Calculations:			
Ultimate Bearing Pressure:	Qu =	1313	psf
Effective Allowable Soil Bearing Pressure:	Qe =	1350	psf
Required Footing Area:	Areq =	15.56	sf
Area Provided:	A =	16.00	sf

Baseplate Bearing:			
Bearing Required:	Bear =	31200	lb
Allowable Bearing:	Bear-A =	99450	lb

Beam Shear Calculations (One Way Shear):			
Beam Shear:	Vu1 =	8613	lb
Allowable Beam Shear:	Vc1 =	29700	lb

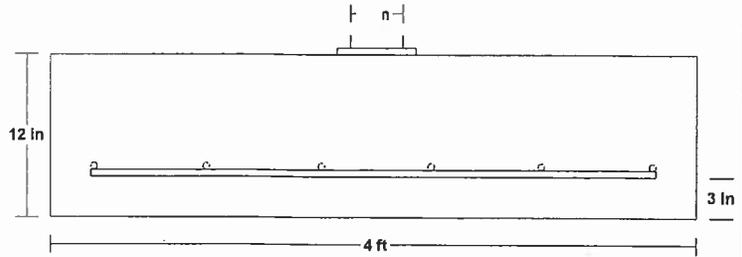
Punching Shear Calculations (Two Way Shear):			
Critical Perimeter:	Bo =	53	in
Punching Shear:	Vu2 =	28823	lb
Allowable Punching Shear (ACI 11-35):	vc2-a =	98381	lb
Allowable Punching Shear (ACI 11-36):	vc2-b =	134888	lb
Allowable Punching Shear (ACI 11-37):	vc2-c =	65588	lb
Controlling Allowable Punching Shear:	vc2 =	65588	lb

Bending Calculations:			
Factored Moment:	Mu =	150231	in-lb
Nominal Moment Strength:	Mn =	339930	in-lb

Reinforcement Calculations:			
Concrete Compressive Block Depth:	a =	0.46	in
Steel Required Based on Moment:	As(1) =	0.51	in2
Min. Code Req'd Reinf. (Shrink./Temp. (ACI-10.5.4):	As(2) =	1.15	in2
Controlling Reinforcing Steel:	As-reqd =	1.15	in2
Selected Reinforcement:	#4's @ 8.0 in. o.c. e/w (6) Min.		
Reinforcement Area Provided:	As =	1.18	in2

Development Length Calculations:			
Development Length Required:	Ld =	15	in
Development Length Supplied:	Ld-sup =	18.5	in

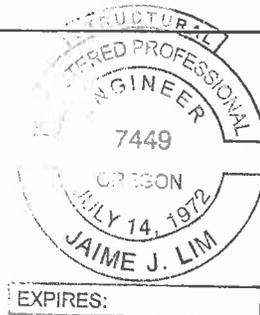
LOADING DIAGRAM



FOOTING LOADING

Live Load:	PL = 15000	lb
Dead Load:	PD = 6000	lb
Total Load:	PT = 21000	lb
Ultimate Factored Load:	Pu = 31200	lb

NOTES



EXPIRES:

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Project: Richard Ahyou
 Location: Footing 2
 Footing
 [2006 International Building Code(2005 NDS)]
 Footing Size: 2.75 FT x 2.75 FT x 12.00 IN
 Reinforcement: #4 Bars @ 6.00 IN. O.C. EW / (5) min.
 Section Footing Design Adequate



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FOOTING PROPERTIES	
Allowable Soil Bearing Pressure:	Qs = 1500 psf
Concrete Compressive Strength:	F'c = 2500 psi
Reinforcing Steel Yield Strength:	Fy = 40000 psi
Concrete Reinforcement Cover:	c = 3 in

FOOTING SIZE	
Width:	W = 2.75 ft
Length:	L = 2.75 ft
Depth:	Depth = 12 in
Effective Depth to Top Layer of Steel:	d = 8.25 in

COLUMN AND BASEPLATE SIZE	
Column Type:	Steel
Column Width:	m = 4 in
Column Depth:	n = 4 in
Baseplate Width:	bsw = 6 in
Baseplate Length:	bsl = 6 in

FOOTING CALCULATIONS	
Bearing Calculations:	
Ultimate Bearing Pressure:	Qu = 1322 psf
Effective Allowable Soil Bearing Pressure:	Qe = 1350 psf
Required Footing Area:	Areq = 7.41 sf
Area Provided:	A = 7.56 sf
Baseplate Bearing:	
Bearing Required:	Bear = 14800 lb
Allowable Bearing:	Bear-A = 99450 lb
Beam Shear Calculations (One Way Shear):	
Beam Shear:	Vu1 = 2579 lb
Allowable Beam Shear:	Vc1 = 20419 lb

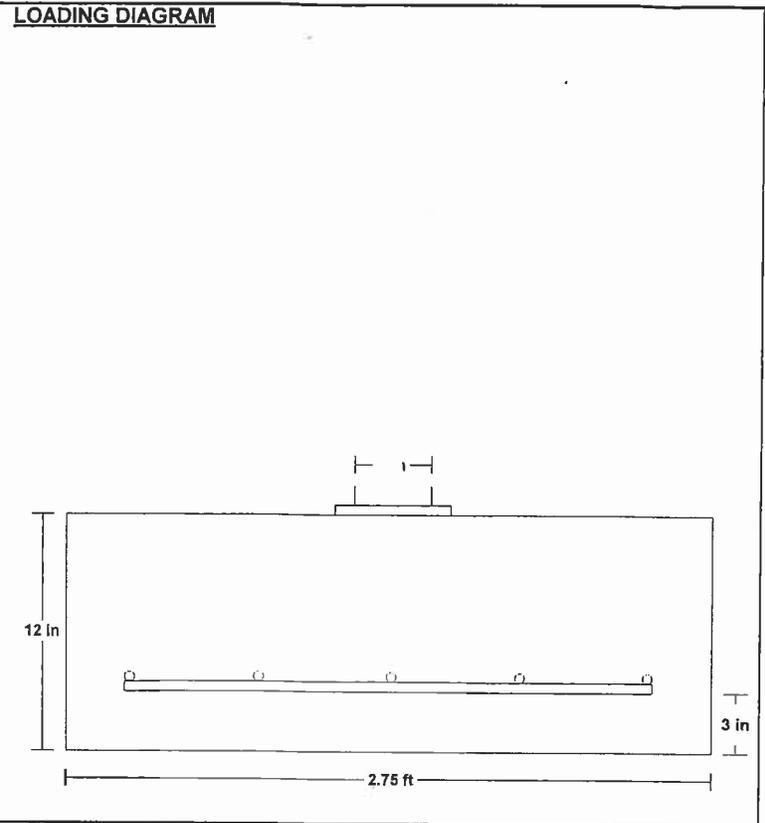
Punching Shear Calculations (Two Way Shear):	
Critical Perimeter:	Bo = 53 in
Punching Shear:	Vu2 = 12414 lb
Allowable Punching Shear (ACI 11-35):	vc2-a = 98381 lb
Allowable Punching Shear (ACI 11-36):	vc2-b = 134888 lb
Allowable Punching Shear (ACI 11-37):	vc2-c = 65588 lb
Controlling Allowable Punching Shear:	vc2 = 65588 lb

Bending Calculations:	
Factored Moment:	Mu = 43952 in-lb
Nominal Moment Strength:	Mn = 281545 in-lb

Reinforcement Calculations:	
Concrete Compressive Block Depth:	a = 0.56 in
Steel Required Based on Moment:	As(1) = 0.15 in2
Min. Code Req'd Reinf. (Shrink./Temp. (ACI-10.5.4):	As(2) = 0.79 in2
Controlling Reinforcing Steel:	As-reqd = 0.79 in2
Selected Reinforcement:	#4's @ 6.0 in. o.c. e/w (5) Min.
Reinforcement Area Provided:	As = 0.98 in2

Development Length Calculations:	
Development Length Required:	Ld = 15 in
Development Length Supplied:	Ld-sup = 11 in

Note: Plain concrete adequate for bending, therefore adequate development length not required.



FOOTING LOADING	
Live Load:	PL = 7000 lb
Dead Load:	PD = 3000 lb
Total Load:	PT = 10000 lb
Ultimate Factored Load:	Pu = 14800 lb

NOTES

Project: Richard Ahyou
 Location: Roof Rafter 1
 Roof Rafter
 [2006 International Building Code(2005 NDS)]
 1.5 IN x 7.25 IN x 15.5 FT (13.5 + 2) @ 16 O.C.
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 30.9%
 Controlling Factor: Moment



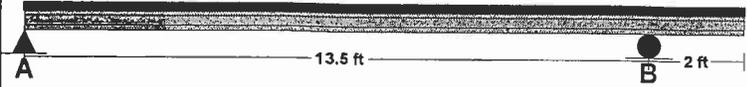
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LOADING DIAGRAM



DEFLECTIONS	Center	Right
Live Load	0.33 IN L/496	0.02 IN L/1588
Dead Load	0.19 in	0.00 in
Total Load	0.51 IN L/316	0.00 IN L/Infinity
Live Load Deflection Criteria: L/240 Total Load Deflection Criteria: L/180		

RAFTER REACTIONS	LOADS	REACTIONS
Upper Live Load @ A	169 plf	225 lb
Upper Dead Load @ A	99 plf	132 lb
Upper Total Load @ A	268 plf	357 lb
Lower Live Load @ B	222 plf	297 lb
Lower Dead Load @ B	133 plf	178 lb
Lower Total Load @ B	356 plf	475 lb

RAFTER SUPPORT DATA	A	B
Bearing Length	0.38 in	0.51 in

RAFTER DATA	Interior	Eave
Span Length	13.5 ft	2 ft
Rafter Pitch	0	:12
Roof sheathing applied to top of joists-top of rafters fully braced.		
Roof Duration Factor	1.15	
Peak Notch Depth	0.00	
Base Notch Depth	0.00	

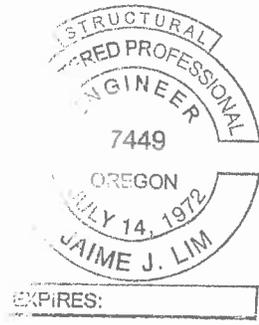
MATERIAL PROPERTIES
 #2 - Douglas-Fir-Larch

	Base Values	Adjusted
Bending Stress:	Fb = 900 psi Cd=1.15 CF=1.20 Cr=1.15	Fb' = 1428 psi
Shear Stress:	Fv = 180 psi Cd=1.15	Fv' = 207 psi
Modulus of Elasticity:	E = 1600 ksi	E' = 1600 ksi
Min. Mod. of Elasticity:	E_min = 580 ksi	E_min' = 580 ksi
Comp. ⊥ to Grain:	Fc ⊥ = 625 psi	Fc ⊥' = 625 psi

Controlling Moment: 1195 ft-lb
 6.75 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2
Controlling Shear: -339 lb
 At a distance d from right support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2, 3

Comparisons with required sections:	Req'd	Provided
Section Modulus:	10.04 in3	13.14 in3
Area (Shear):	2.46 in2	10.88 in2
Moment of Inertia (deflection):	27.13 in4	47.63 in4
Moment:	1195 ft-lb	1564 ft-lb
Shear:	-339 lb	1501 lb

RAFTER LOADING	
Uniform Floor Loading	
Roof Live Load: LL =	25 psf
Roof Dead Load: DL =	15 psf
Slope Adjusted Spans And Loads	
Interior Span: L-adj =	13.5 ft
Eave Span: L-Eave-adj =	2 ft
Rafter Live Load: wL-adj =	33 plf
Eave Live Load: wL-Eave-adj =	33 plf
Rafter Dead Load: wD-adj =	20 plf
Rafter Total Load: wT-adj =	53 plf
Eave Total Load: wT-Eave-adj =	53 plf



NOTES

Project: Richard Ahyou
 Location: Deck Joist 1 2 x 12 @ 16" o/c
 Multi-Span Floor Beam
 [2006 International Building Code(2005 NDS)]
 1.5 IN x 11.25 IN x 11.0 FT (10 + 1)
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 83.1%
 Controlling Factor: Moment



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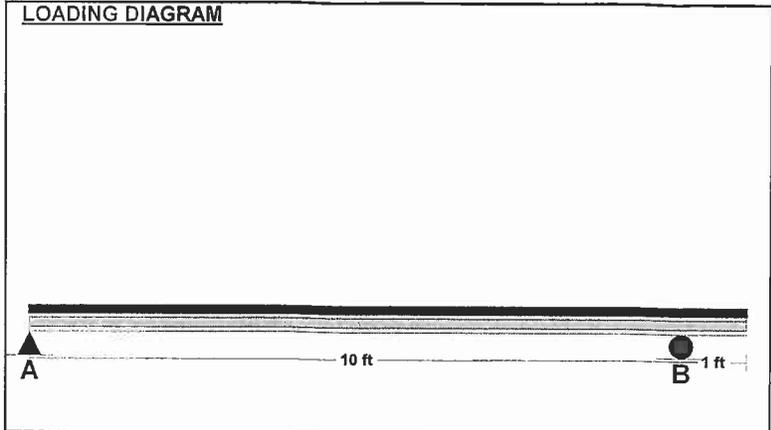
DEFLECTIONS	Center		Right	
Live Load	0.06	IN L/1889	-0.02	IN L/590
Dead Load	0.02	in	-0.01	in
Total Load	0.08	IN L/1466	-0.03	IN L/460
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240				

REACTIONS	A	B
Live Load	402 lb	486 lb
Dead Load	118 lb	144 lb
Total Load	520 lb	630 lb
Bearing Length	0.55 in	0.67 in

BEAM DATA	Center	Right
Span Length	10 ft	1 ft
Unbraced Length-Top	0 ft	0 ft
Unbraced Length-Bottom	10 ft	1 ft
Floor Duration Factor	1.00	
Notch Depth	0.00	

MATERIAL PROPERTIES
 #2 - Douglas-Fir-Larch

	Base Values	Adjusted
Bending Stress:	Fb = 900 psi Cd=1.00 CF=1.00	Fb' = 900 psi
Shear Stress:	Fv = 180 psi Cd=1.00	Fv' = 180 psi
Modulus of Elasticity:	E = 1600 ksi	E' = 1600 ksi
Min. Mod. of Elasticity:	E_min = 580 ksi	E_min' = 580 ksi
Comp. ⊥ to Grain:	Fc ⊥ = 625 psi	Fc ⊥' = 625 psi



FLOOR LOADING	Center	Right
Floor Live Load	FLL = 60 psf	60 psf
Floor Dead Load	FDL = 15 psf	15 psf
Floor Tributary Width Side One	TW1 = 0.7 ft	0.7 ft
Floor Tributary Width Side Two	TW2 = 0.7 ft	0.7 ft
Wall Load	WALL = 0 plf	0 plf

BEAM LOADING	Center	Right
Reduced Floor Live Load	60 psf	60 psf
Total Live Load	80 plf	80 plf
Total Dead Load	20 plf	20 plf
Beam Self Weight	4 plf	4 plf
Total Load	104 plf	104 plf

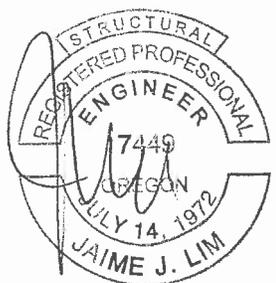
Controlling Moment: 1296 ft-lb
 5.0 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2

Controlling Shear: -432 lb
 At a distance d from right support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2, 3

Comparisons with required sections:

	Req'd	Provided
Section Modulus:	17.28 in3	31.64 in3
Area (Shear):	3.6 in2	16.88 in2
Moment of Inertia (deflection):	54.26 in4	177.98 in4
Moment:	1296 ft-lb	2373 ft-lb
Shear:	-432 lb	2025 lb

NOTES



EXPIRES: _____

Project: Richard Ahyou
 Location: Deck Joist 2 @ 8" o/c Hot Tub Support Joist
 Multi-Loaded Multi-Span Beam
 [2006 International Building Code(2005 NDS)]
 1.5 IN x 11.25 IN x 11.0 FT (10 + 1)
 #2 - Douglas-Fir-Larch - Dry Use
 Section Adequate By: 1.2%
 Controlling Factor: Moment



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DEFLECTIONS	Center	Right
Live Load	0.12 IN L/1000	-0.04 IN L/297
Dead Load	0.02 in	-0.01 in
Total Load	0.14 IN L/844	-0.05 IN L/252
Live Load Deflection Criteria: L/360 Total Load Deflection Criteria: L/240		

REACTIONS	A	B
Live Load	506 lb	956 lb
Dead Load	119 lb	176 lb
Total Load	625 lb	1132 lb
Bearing Length	0.67 in	1.21 in

BEAM DATA	Center	Right
Span Length	10 ft	1 ft
Unbraced Length-Top	0 ft	0 ft
Unbraced Length-Bottom	10 ft	1 ft
Live Load Duration Factor	1.00	
Notch Depth	0.00	

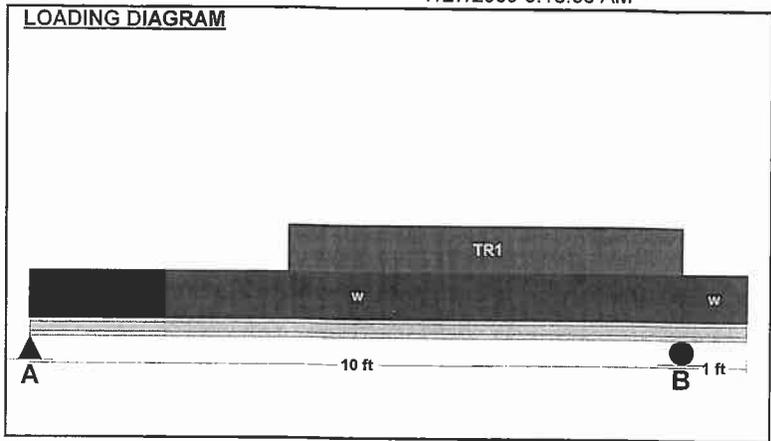
MATERIAL PROPERTIES

#2 - Douglas-Fir-Larch

	Base Values	Adjusted
Bending Stress:	Fb = 900 psi Cd=1.00 CF=1.00	Fb' = 900 psi
Shear Stress:	Fv = 180 psi Cd=1.00	Fv' = 180 psi
Modulus of Elasticity:	E = 1600 ksi	E' = 1600 ksi
Min. Mod. of Elasticity:	E_min = 580 ksi	E_min' = 580 ksi
Comp. ⊥ to Grain:	Fc ⊥ = 625 psi	Fc ⊥' = 625 psi

Controlling Moment: 2345 ft-lb
 5.6 Ft from left support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2
Controlling Shear: -854 lb
 At a distance d from right support of span 2 (Center Span)
 Created by combining all dead loads and live loads on span(s) 2, 3

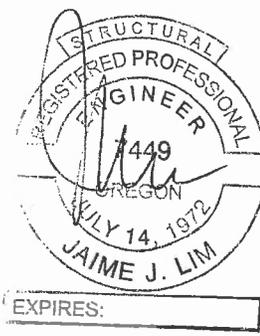
Comparisons with required sections:	Req'd	Provided
Section Modulus:	31.27 in ³	31.64 in ³
Area (Shear):	7.12 in ²	16.88 in ²
Moment of Inertia (deflection):	107.95 in ⁴	177.98 in ⁴
Moment:	2345 ft-lb	2373 ft-lb
Shear:	-854 lb	2025 lb



UNIFORM LOADS	Center	Right
Uniform Live Load	40 plf	40 plf
Uniform Dead Load	15 plf	15 plf
Beam Self Weight	4 plf	4 plf
Total Uniform Load	59 plf	59 plf

TRAPEZOIDAL LOADS - CENTER SPAN	
Load Number	One
Left Live Load	170 plf
Left Dead Load	15 plf
Right Live Load	170 plf
Right Dead Load	15 plf
Load Start	4 ft
Load End	10 ft
Load Length	6 ft

NOTES



5TH AVE

178' ELEV.

OVERHEAD UTILITY LINES

POWER POLE

SIDEWALK

SITE PLAN
 SCALE: 1"=10'-0"

PROPERTY ADDRESS:
 2155 5TH AVE
 WEST LINN
 OREGON 97068

LOT SIZE: 50' X 200'

LEGEND:

- PROPERTY LINE
- UTILITIES

12" DBH CHERRY

PAVED WALK

COVERED PORCH

4" DBH MAPLE



CONC.

PORCH

2155 5TH AVE
 WEST LYNN, OR
 97068

PAVED DRIVEWAY

A.C.

168' ELEV.

CONTAINMENT FOR CONSTRUCTION WASTE

EXISTING ELEVATED DECK
ELEVATION +10'

EXISTING PAVED PATIO
ELEVATION 0'

EXISTING LOWER DECK
ELEVATION +2'

5TH A

178' ELEV.

OVERHEAD UTILITY LINES

POWER POLE

SIDEWALK

SITE PLAN

SCALE: 1"=10'-0"

12" DBH CHERRY

PAVED WALK

COVERED PORCH



PROPERTY ADDRESS:
2155 5TH AVE
WEST LINN
OREGON 97068

LOT SIZE: 50' X 200'

4" DBH MAPLE

CONC.

LEGEND:

----- PROPERTY LINE

----- UTILITIES

PORCH

PAVED DRIVEWAY

2155 5TH AVE
WEST LYNN, OR
97068

A.C.

168' ELEV.

CONTAINMENT FOR
CONSTRUCTION
WASTE

EXISTING
ELEVATED
DECK
ELEVATION +10'

EXISTING
PAVED
PATIO
ELEVATION 0'

EXISTING
LOWER
DECK
ELEVATION +2'

100' MARK OF
200' LONG PROPERTY

158' ELEV.



36" DBH
OAK